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STEREOLOGICAL ANALYSIS OF PARTICLE CHARACTERISTICS

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ABSTRACT

Important characteristics of particles are their size, specific surface and shape. The stereological parameters available to quantify these three attributes are discussed, both for loose particles and particles contained within a matrix. A shape parameter for particle roughness is developed, showing that a more complicated function expresses the roughness characteristics better than a simple function.

INTRODUCTION

Traditionally, it appears that microscopical studies of loose particles have tended to rely more on the projected characteristics than on the sectioned quantities. Thus, stereology, which leans heavily on both methods of observation, can be considered to bring another dimension to the quantitative study of particle characteristics. Both two-dimensional and three-dimensional quantities are considered in discussing the choices available for size, specific surface and shape parameters. These three topics are discussed in turn.

SIZE

The 'size' of a particle, or of a system of particles, can be expressed in many ways. Generally, we define some geometrical parameter related to 'size', such as a linear, areal or volume-based measure. Unfortunately, the 'diameter' as a measure of size is meaningless except for circles and spheres. For other figures or objects, the parameter actually selected must be clearly defined. We would like

the size parameter that we select to be free of $\underbrace{a\ priori}$ assumptions about shape, if at all possible. Moreover, it should have a unique value that is reproducible, easily measured, and related to the three-dimensional particle quantities.

The most general and assumption-free choice of linear size parameter is the mean intercept length, \overline{L}_2 (in the section plane), or \overline{L}_3 (in three dimensions). The basic defining equation is

$$\overline{L}_{2} = \overline{L}_{3} = \sum L_{i} / \sum n_{i}$$
 (1)

which states that the sum of many linear intercepts (Σ L.) taken along random test lines, divided by the total number of intercepts (Σ n_i), is the mean intercept length (either two- or three-dimensional). This definition applies equally to a single particle or a system of particles, and the particles can have any shape (convex and/or concave).

Experimentally, we obtain the mean intercept length from embedded particles by the relationship

$$\overline{L}_2 = \overline{L}_3 = L_L / N_L = P_P / N_L$$
 (2)

where L_L , the intercept length per unit length of test line, is equal to P_p , the point ratio of particles hit to the total number of grid points applied, and N_L is the number of intercepts of particles per unit length of test lines. \overline{L}_3 is related to other three-dimensional quantities, such as the specific surface S/V, and is completely general and independent of particle size, shape and complexity.

When the particles are convex in shape (or reasonably equiaxed), additional linear size parameters are available. For example, we can use \overline{d} or \overline{D} , the mean tangent diameters in the section plane or in space, respectively, or \overline{H}' , the mean tangent height in the projection plane. Frequently, the minimum or maximum values of linear size parameter are desired. For convex bodies we have

$$D_{\text{max}} = (\overline{L}_3)_{\text{max}} = d_{\text{max}}$$
 (3)

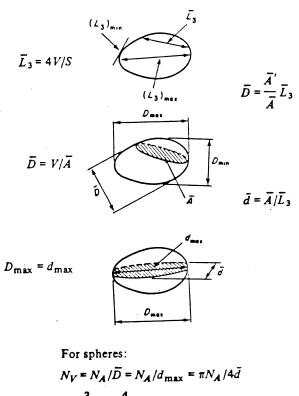
and for spheres of diameter D, we can write

$$D = d_{\max}. \tag{4}$$

The maximum and minimum linear size parameters for particles of known shape may be calculated. Note that the measured values of intercept lengths vary between zero and some maximum value, while the various measured tangent diameters vary between a non-zero minimum value and a maximum.

$$\overline{L}_3 < \overline{D}$$
. (5)

Some of the interrelationships among these size parameters are shown in Figure 1.



$$N_V = N_A / \bar{D} = N_A / d_{\text{max}} = \pi N_A / 4 \bar{d}$$

 $\bar{D} = \frac{3}{2} \bar{L}_3 = \frac{4}{\pi} \bar{d} = d_{\text{max}}$

Fig. 1. Length parameters in convex bodies

In addition to linear measures of particle size, areal and volume-based definitions of size are also possible. size definitions can employ A or A', the sectioned or projected area, or the mean or maximum values. In the twodimensional section plane, the mean intercept area is given by

$$\overline{A} = A_A N_A = P_P N_A, \qquad (6)$$

and in the projection plane, the mean projected area is

$$\overline{A}^{\dagger} = A_{A}^{\dagger} / N_{A}^{\dagger} = P_{P}^{\dagger} / N_{A}^{\dagger}. \tag{7}$$

A' is of importance because it is related to sieve size. A spatial quantity that may be used for a size parameter is S, the surface area of the particle. For a convex particle we use the Cauchy expression

$$S = 4\overline{A}', \tag{8}$$

or a variant of Eq. 8 for a system of particles,

$$S_{V} = 4A_{A}^{\prime}/t \tag{9}$$

where t is the foil thickness and A_{A}^{\bullet} is the area fraction in the projection plane. Also, the average surface area per particle, \overline{S} , is given simply by the defining equation

$$\overline{S} = S_{V} / N_{V}. \tag{10}$$

The definition of size in terms of volume has its staunch advocates. V, or V, has the advantage of being a true three-dimensional quantity, independent of shape or orientation. For irregularly-shaped particles, the volume size parameter suffers the disadvantage of being difficult to determine directly, and requires either weakening assumptions or laborious experimental work. Moreover, it offers no information on particle shape.

In general, the mean volume is defined by

$$\overline{V} = V_{V} N_{V} = P_{P} N_{V}$$
(11)

where N_{V} , the number of particles per unit test volume, is difficult to obtain.

For convex particles, the three types of parameters discussed above are related by extremely general equations. Thus we have

$$\bar{d} = \bar{A}/\bar{L}_3 = \bar{A}'/\bar{D} = \bar{L}_p/\pi$$
 (12)

$$\overline{D} = V/\overline{A} = \overline{A}'\overline{L}_3/\overline{A} = \overline{H}'$$
(13)

$$\overline{A} = V/\overline{D} = \overline{L}_3 \overline{L}_2' = \overline{A}' \overline{L}_3 / \overline{H}'$$
 (14)

$$\overline{A'} = V/\overline{L}_3 = \overline{H'}\overline{L}_2 = S/4 \tag{15}$$

The mean intercept length and volume relationships can also be obtained from these equations. If a specific particle shape is assumed, these general equations can be expressed explicitly in terms of a particle dimension or the other quantities. For example, for a sphere of diameter D, we have

$$D = 3\overline{L}_3/2 = 4\overline{d}/\pi \tag{16}$$

$$\overline{A} = 2\overline{A}'/3 \tag{17}$$

$$V = \pi r^2 \overline{L}_3, \tag{18}$$

etc. Moreover, only V, S and \overline{D} need be known in order to calculate any of the above stereological quantities (2d or 3-d) for any convex body.

SPECIFIC SURFACE

This ubiquitous parameter appears to exert a decisive influence on the properties of many particulate systems. The three-dimensional specific surface is defined for a single particle by S/V, where the surface and volume terms refer to the particle itself. For a system of particles, we may need $\overline{S/V}$. The specific surface is related to the mean intercept length by

$$\frac{S}{V} = \frac{4}{\overline{L}_3} \tag{19}$$

and also

$$\frac{S}{V} = \frac{S_V}{V_V} = \frac{\overline{S}}{\overline{V}} = \frac{4}{\overline{L}_3} = \frac{4N_L}{P_P}$$
 (20)

If loose particles are embedded and sectioned, a two dimensional analogue to S/V is obtained, i.e., $\overline{L}/\overline{A}$, which is the mean perimeter length divided by the mean sectioned area. These two ratios are related through

$$\frac{\overline{S}}{\overline{V}} = \frac{4}{\pi} \frac{\overline{L}}{\overline{A}}.$$
 (21)

Figure 2 summarizes the equations for specific surface applicable to two important types of particulate systems. On the left is a system of particles enbedded randomly in a matrix. The other type of system, shown on the right, consists of loose, individual particles. Definitions for S and V are given for both types. It can be seen that the specific surface of sectioned particles in a matrix can be obtained by combined point and intersection counts, while for loose particles the relatively inaccessible total surface area and volume of particles are needed.

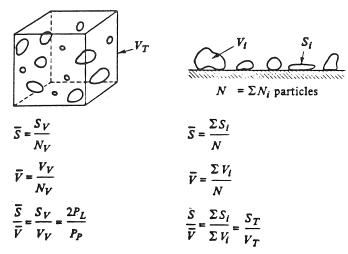


Fig. 2. Determination of specific surface

Although the ratio S/V is determined readily enough through the basic Equations 19, 20 or 21, it is more difficult to obtain the values of S and V separately. As mentioned above, S may be determined through Equation 8, while V may possibly be calculated through Eqs. 11 or 13, although $\overline{\rm D}$ or N $_{\rm V}$ are difficult three-dimensional quantities to obtain.

In these examples, note the difference between \mathbb{S}_{v} and \mathbb{S}/v . The first term is the standard stereological quantity $(\equiv \sum \mathbb{S}_{i}/\mathbb{V}_{T})$, equal to $2\mathbb{P}_{L}$, and refers to the total surface area of the particles divided by the test volume (particles plus matrix). The second term is the specific surface, where the particle surface area is divided by the particle volume only. Accordingly, $\overline{\mathbb{S}/V}$ for embedded particles is equal to $2\mathbb{P}_{L}/\mathbb{P}_{p}$.

SHAPE

The idea of 'shape' is one of the most difficult concepts to define, let alone quantify. Shape parameters are generally used to express some particle attribute such as roughness, roundness, acicularity, etc. Although shape parameters are preferably dimensionless, nevertheless they are composed largely of metric terms, e.g., length, surface area, and/or volume. Curvature of lines and/or surfaces and topological quantities, i.e., the <u>number</u> of corners, edges, faces and/or bodies, may also find application in a shape parameter.

Sometimes simple ratios or products of terms may be combined to produce a satisfactory shape parameter. For example, useful combinations are L/W, the length-to-width ratio; L_p/L_2 , the perimeter length divided by intercept length; L_2/A , the perimeter length squared divided by the L_2/A , the area times the line curvature squared. Frequently, however, more complicated parameters may be needed to express the shape characteristics of interest.

Figure 3 defines the mean particle area \overline{A} and the equivalent circle area A_{eq} , as well as the equivalent diameter d_{eq} and equivalent perimeter length $(L_p)_{eq}$. Many shape parameters are based on ratios of the microstructural quantity. For example, we might wish to use $(\overline{L}_p)_{meas}/(L_p)_{eq}$, etc.

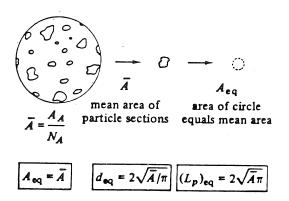


Fig. 3. Quantities calculated from equivalent area circle

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Sometimes we must combine several stereological quantities in order to relate all the important shape characteristics to the particle properties or behavior. Two-dimensional quantities that are useful in shape studies are

$$\bar{A}$$
, \bar{L}_2 , \bar{L}_p , \bar{d} and \bar{k}_L

while three-dimensional quantities are

$$V$$
, S , \overline{D} , \overline{L}_3 , and \overline{K}_S ,

where \overline{k}_L , and K are the mean curvature of lines in a plane and the average mean curvature of surfaces, respectively. Typical interconversions among these quantities are given in Table I. Thus, shape parameters can be expressed in terms of either two- or three-dimensional quantities.

TABLE I

BASIC RELATIONSHIPS FOR SHAPE PARAMETERS	
<u>Planar Quantities</u>	Spatial Quantities
$\bar{A} = \frac{V}{\bar{D}} = \frac{A_A}{N_A}$	$V = \overline{L}_2 \overline{A}' = \frac{V_V}{N_V}$
$\overline{L}_p = \frac{\pi S}{4 \overline{D}} = \frac{L_A}{N_A}$	$S = 4\overline{A}' = \frac{4N_L}{N_V}$
$\bar{d} = \frac{S}{4\bar{D}} = \frac{N_L}{N_A}$	$\overline{D} = \frac{\overline{A}'}{\overline{d}} = \frac{N_A}{N_V}$
$\overline{L}_2 = \frac{4V}{S} = \frac{L_L}{N_L}$	$\overline{L}_3 = \frac{\overline{A}}{\overline{d}} = \frac{L_L}{N_L}$
$\overline{k}_L = \frac{8\overline{D}}{S} = \frac{2N_A}{N_L}$	$\overline{K}_s = \frac{\pi}{2\overline{d}} = \frac{\pi N_A}{2N_L}$

An example of this procedure is afforded by an analysis of a series of particle silhouettes shown in Figure 4. In order to express the particle 'roughness', we might try the ratio L/A. However, additional information is desirable, such as p the number of projections (or 'hills') around the

perimeter. The latter is related to the number of inflection points (I) and thereby to the curvature. Additionally, as the particles show more elongation, the aspect ratio (Q) becomes important.

Thus the shape parameters progress from $\frac{\Delta(\text{L}_p/A)}{\text{I}}, \text{ where } \Delta(\text{L}_p/A) = (\text{L}_p/A)_{\text{meas}} - (\text{L}_p/A)_{\text{and I is obtained readily by counting hills according to I = 2N}_{\text{hills}}; \text{ then to}$ $\frac{\Delta(\text{L}_p/A)}{(\text{L}_p/A)}, \text{ which gives the relative change in L}_p/A \text{ with respect to the equivalent area circle; and finally to}$ $\frac{\Delta(\text{L}_p/A) \cdot \text{Q}}{(\text{L}_p/A) \cdot \text{Q}}, \text{ which introduces the aspect ratio Q.}$

Numerical results obtained with these three shape parameters are given in turn below each figure in Figure 4. Only for the third shape parameter do the values proceed systematically as the apparent roughness increases. Thus,

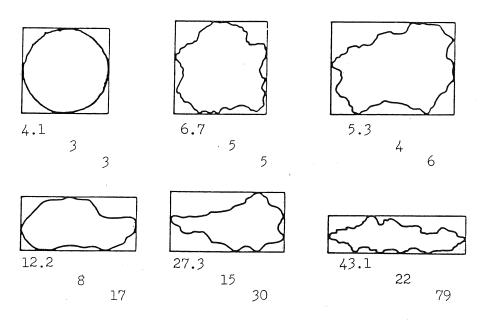


Fig. 4. Variation of roughness parameters with particle profile shape

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it appears that this complexing procedure has merit. Without doubt, more refined analyses should lead to even better results.

CONCLUSIONS

Stereological quantities that express size, specific surface and shape are given for loose particles or loose particles mounted in a resin matrix. The mean intercept length, L_2 , appears to represent 'size' best, while the specific surface, S/V, is given readily by a combined intersection and point count, $2P_p$. The 'shape' of particle silhouettes is expressed by a combined parameter that includes the (L_p/A) ratio; I, the number of inflection points; and Q, the aspect ratio.

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